## SOURCE ON AN INFINITE CYLINDER

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The temperature field produced in an infinite circular cylinder on application of a temperature step to a bounded portion of its surface is analyzed by successive application of Fourier and Laplace transformations. Curves are given showing the time dependence of the axial and radial temperature distributions for a temperature step applied to a narrow annular portion of the surface.

In the present article we analyze the temperature field produced in an infinite cylinder $(0 \leq \rho \leq a$, $0 \leq \varphi \leq 2 \pi,-\infty<z<\infty)$ when a bounded portion of its surface is instantaneously raised to a temperature $\mathrm{T}_{0}$ which is subequently maintained constant. The temperature of the rest of the surface of the cylinder is taken to be always zero.

We thus require to solve the boundary problem

$$
\begin{equation*}
\Delta T=\frac{1}{c} \frac{\partial T}{\partial t} \tag{1}
\end{equation*}
$$

where $\Delta=\left(\partial^{2} / \partial \rho^{2}\right)+(1 / \rho)(\partial / \partial \rho)+\left(1 / \rho^{2}\right)\left(\partial^{2} / \partial \varphi^{2}\right)+\left(\partial^{2} / \partial z^{2}\right)$ is the Laplace operator, and cis the thermal conductivity, For $t \leq 0$ the temperature $T=0$ within and on the surface of the cylinder, and for $t>0$

$$
T_{\rho=a}=\left\{\begin{array}{c}
\frac{N}{4 b h}, \quad \text { when }\left\{\begin{array}{l}
|z| \leqslant h \\
|\varphi| \leqslant \alpha
\end{array}\right.  \tag{2}\\
0 \text { for all other } z \text { and } \varphi
\end{array}\right.
$$

where $N / 4 b h=T_{0}=$ const; $N$ is a constant of suitable dimensionality; $2 h$ is the linear extent of the source as measured along the cylinder (at $\rho=a$ ); and $2 \mathrm{~b}=2 \alpha a$ is the linear extent of the source as measured around the perimeter of the cylinder.

Further, the function $T$ and its derivatives are required to approach zero as $|z| \rightarrow \infty$.
We express condition (2) in the form of a Fourier series:

$$
T_{\rho=a}=\left\{\begin{array}{cl}
\frac{N}{4 b h} \sum_{n=0}^{\infty} \frac{\sin (n a) \cos (n \varphi)}{\pi \varepsilon_{n} n} & \text { for }|z| \leqslant h \\
0 & \text { for }|z|>h
\end{array}\right.
$$

where $\varepsilon=2$ for $n=0$ and $\varepsilon=1$ for $\mathrm{n}=1,2,3, \ldots$
We now apply in succession in Eq. (1) and condition (2) a Fourier transformation [1] with respect to $z$ and a Laplace transformation [2] with respect to time $t$. On performing the necessary calculations, we arrive at the following expression for the temperature field in the cylinder:

$$
\begin{equation*}
T=\frac{N}{b} \sum_{n=0}^{\infty} \sum_{m=1}^{\infty} \frac{\sin (n \alpha) \cos (n \varphi)}{\pi \varepsilon_{n} n} \frac{J_{n}\left(\frac{\beta_{n}^{m}}{a} \rho\right)}{J_{n+1}\left(\beta_{n}^{m}\right)}\left[F_{n}^{m}+\Phi_{n}^{m}\right] \tag{3}
\end{equation*}
$$

Taganrog Radio Engineering Institute. Translated from Inzhenerno-Fizicheskii Zhurnal, Vol. 17, No. 4, pp. 730-732, October, 1969. Original article submitted June 18, 1968.
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Fig. 1. (a) Axial and (b) radial temperature distributions for various values of time t : 1) $\mathrm{t}=1 \mathrm{sec}$; 2) 1.75 ; 3) 3.0 ; 4) $\mathrm{t}=\infty$, $a=1 \mathrm{~cm} ; \mathrm{c}=0.12 \mathrm{~cm}^{2} / \mathrm{sec}, \mathrm{z}=0.6(\mathrm{t}, \mathrm{sec} ; \rho, \mathrm{cm} ; a, \mathrm{~cm} ; \mathrm{c}$, $\left.\mathrm{cm}^{2} / \mathrm{sec} ; \mathrm{z}, \mathrm{cm}\right)$.

Here

$$
\begin{gathered}
F_{n}^{m}=\frac{\operatorname{sh}\left(\frac{\beta_{n}^{m}}{a} \rho\right)}{\beta_{n}^{m h}} \exp \left(-\frac{\beta_{n}^{m}}{a} z\right) ; \\
\Phi_{n}^{m}=\frac{1}{4 a} \sum_{k=0}^{1} \frac{1}{h} \int_{0}^{i}\left\{\exp \left[-\frac{\beta_{n}^{m}}{a}\left(z+(-1)^{k} \theta\right)\right]\right. \\
\left.\times \operatorname{erfc}\left[\sqrt{c t} \frac{\beta_{n}^{m}}{a}-\frac{z+(-1)^{k} \theta}{2 \sqrt{c t}}\right]+\exp \left[\frac{\beta_{n}^{m}}{a}\left(z+(-1)^{k} \theta\right)\right] \operatorname{erfc}\left[\sqrt{c t} \frac{\beta_{n}^{m}}{a}+\frac{z+(-1)^{k} \theta}{2 \sqrt{c t}}\right]\right\} d \theta .
\end{gathered}
$$

Formula (3) simplifies somewhat for an annular source $2 b=2 \pi a$ for smallaxial extent, i.e., $h \ll 1$. In this case

$$
\begin{gather*}
T=\frac{N}{2 \pi} \sum_{m=1}^{\infty} \frac{J_{0}\left(\frac{\beta_{0}^{m i}}{a} \rho\right)}{J_{1}\left(\beta_{0}^{m}\right)} \exp \left(-\frac{\beta_{0}^{m}}{a} z\right)\left\{1-\frac{1}{2 a}\right. \\
\left.\times\left[\operatorname{erfc}\left(\sqrt{c t} \frac{\beta_{0}^{m}}{a}-\frac{z}{2 \sqrt{c t}}\right)+\exp \left(2 \frac{\beta_{0}^{m}}{a} z\right) \operatorname{erfc}\left(\sqrt{c t} \frac{\beta_{0}^{m}}{a}+\frac{z}{2 \sqrt{c t}}\right)\right]\right\} \tag{4}
\end{gather*}
$$

The axial and radial temperature distributions calculated through formula (4) are shown in Fig. 1a and b .

As can be seen from the curves, there is a considerable delay in the heating of points $\rho=0$ (Fig. ib) in the initial period following the application of the temperature step. The temperature subsequently builds up to its limiting value.

The thermal fields produced by a pulsed source can be analyzed with the aid of solutions (3) and (4). The technique is described in [3].

Analogous methods were used in [4] to study periodic thermal fields in a cylinder with second-order boundary conditions.

NOTATION
$\rho, \varphi, \mathrm{z}$ are the cylindrical coordinates;
$a \quad$ is the radius of the cylinder;
$2 h, 2 b$ are the linear dimensions of the source;
$\mathrm{T}_{0} \quad$ is the temperature of the source;
c is the thermal conductivity;
$t$ is the time;
$\Delta \quad$ is the Laplace operator;

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